Seismic Base Isolation For Earthquake Resistant Structure

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Abstract - ETABS are mostly used to design the building structure. This software is used to design base isolated structure and compare with conventional structure.

The present study is based on the comparative study of fixed base building and isolated base building.

1) INTRODUCTION
Base isolation, also known as seismic base isolation or base isolation system, is one of the most popular means of protecting a structure against earthquake forces. It is a collection of structural elements which should substantially decouple a superstructure from its substructure resting on a shaking ground thus protecting a building or non-building structure's integrity.

Base isolation is one of the most powerful tools of earthquake engineering pertaining to the passive structural vibration control technologies. It is meant to enable a building or non-building structure to survive a potentially devastating seismic impact through a proper initial design or subsequent modifications. In some cases, application of base isolation can raise both a structure's seismic performance and its seismic sustainability considerably. Contrary to popular belief base isolation does not make a building earthquake proof.

Base isolation system consists of isolation units with or without isolations components, where:

1. Isolation units are the basic elements of a base isolation system which are intended to provide the aforementioned decoupling effect to a building or non-building structure.
2. Isolation components are the connections between isolation units and their parts having no decoupling effect of their own.

Isolation units could consist of shear or sliding units.

Base isolation is not suitable for all buildings. Mostly low or medium rise building rested on hard strata underneath, high rise building or building resting on soft strata are not suitable for base isolation.
2) **AIM AND OBJECTIVE**

- To prepare earthquake resistant building.
- To analyze the seismic effect on base isolated structure.
- To study the strength and applicability of base isolation system.
- To estimate the cost difference between normal structure and base isolated structure.
- To design base isolators.
- To check the stability of base isolation.

3) **DESIGN OF BASE ISOLATOR**

- This maximum vertical reaction of fixed base building is 2800 KN for internal column and 2007.71 KN for external column is considered as supporting weight of LRBs.
- Target period (2.5 seconds) and the effective damping $\beta$. $\beta$ is assumed to be 5% for reinforced concrete structure according to IS 1893:2002 clause 7.8.2.1
- Spectral acceleration from the response spectrum graph in relation with the period $T = 1$ sec is found to be 0.56 and damping factor for $0.05(\beta)$ is 1 from table 3, IS 1893:2002.
- **Bearing stiffness:**

1. For rubber bearing

   \[
   K_H^E = \left(\frac{2\pi}{T_{EFF}}\right)^2 \times \frac{W_i}{g}
   \]

   \[
   K_H^E = \left(\frac{2\pi}{2.5}\right)^2 \times \frac{2800}{9.81}
   \]

   \[
   K_H^E = 1292.8 \text{ KN/M}
   \]

   \[
   K_H^I = \left(\frac{2\pi}{2.5}\right)^2 \times \frac{2007.71}{9.81}
   \]

   \[
   K_H^I = 1802.66 \text{ KN/M}
   \]

- First estimation of design displacement

   \[
   D_{bd} = \frac{g \times C_D \times T_{EFF}}{4 \times \pi^2 \times B}
   \]

   \[
   D_{bd} = \frac{9.81 \times 0.56 \times 2.5}{4 \times \pi^2 \times 1}
   \]

   \[
   D_{bd} = 0.347 \text{ M}
   \]

   Assuming total rubber thickness $t_r = 200$mm with shear modules 0.4MPa for external column and 1MPa for internal column.

   Hence,

   \[
   K_H^E = \frac{G_i \times A}{t_r}
   \]

   \[
   K_H^E = 1292.8 \text{ KN/M}
   \]

   SO,

   \[
   A = \frac{t_r \times K_H^E}{G_i}
   \]

   \[
   A = \frac{0.2 \times 1292.8 \times 10^3}{0.4 \times 10^6}
   \]

   \[
   A = 0.646 \text{ M}^2
   \]

   And hence diameter,

   \[
   \phi = \left(\frac{4 \times A}{\pi}\right)^{\frac{1}{2}}
   \]

   \[
   \phi = 0.907 \text{ M}
   \]

   Taking $\phi = 0.9m$ and $A = 0.636 \text{ m}^2$
Actual bearing stiffness

\[ K_{H}^E = \frac{G_{t} \times A}{t_{r}} \]

\[ K_{H}^E = \frac{0.4 \times 0.636}{0.2} \]

\[ K_{H}^E = 1.272 \text{ MN/m} \]

And,

\[ K_{H}^l = \frac{G_{t} \times A}{t_{r}} \]

\[ K_{H}^l = \frac{4 \times 0.636}{0.2} \]

\[ K_{H}^l = 3.18 \text{ MN/m} \]

Composite stiffness

\[ K_{H} = 16 \times K_{H}^E + 9 \times K_{H}^l \]

Therefore,

\[ \omega^2 = \frac{48.452 \times 10^6}{1292.8 \times 10^3} \]

\[ \omega^2 = 37.47 \]

\[ \omega = 6.12 \]

\[ T = \frac{2\pi}{\omega} \]

\[ T = 1.02 \]

So,

\[ D_D = \frac{9.81 \times 0.56 \times 1.02}{4 \times 3.14^2 \times 1} = 0.141 \text{ m} \]

Allowance for torsion

\[ D_T = D \left(1 + Y \frac{12e}{b^2 + d^2}\right) \]

Where \( b \) = dimension of shorter side = 16

\( Y = d/2 = 8 \)

\( d = 16 \)

\( e = 0.05 \) times longer direction = 0.05 \( \times 16 = 0.8 \)

\[ D_T = D \left(1 + 8 \frac{12 \times 0.8}{16^2 + 16^2}\right) \]

\[ D_T = 0.162 \text{ m} \]

Elastic base shear

\[ V_S = \frac{K_{H} \times D_D}{R_{WC}} \]

\[ V_S = \frac{48.45 \times 0.141}{2} \]

\[ V_S = 3.41 \times 10^6 N \]
• **Bearing details**

Assume $f_v = 10 \text{ Hz}$

And

\[ s = \frac{1}{\sqrt{6}} \times \frac{f_v}{f_h} \]

\[ s = \frac{1}{\sqrt{6}} \times \frac{10}{2.39} \]

\[ s = 10 \]

To calculate the vertical frequency and the buckling load for bearing, we use small strain shear modulus for each rubber such as 20%.

So,

$G_{0.2}^A = 0.7 \text{ MPa AND } G_{0.2}^B = 1.4 \text{ MPa}$

Assuming $K = 2000 \text{ MPa}$

\[ E_c = \frac{6GS^2K}{6GS^2 + K} \]

$E_c^A = \frac{6 \times 0.7 \times 10^2 \times 2000}{420 + 2000} = 347 \text{ MN/m}^2$

$E_c^B = \frac{0.4 \times 100 \times 200}{2840} = 592 \text{ MN/m}^2$

Composite $K_H = (16 \times 347 + 9 \times 592)^A_{TR}$

$K_H = (16 \times 347 + 9 \times 592)^{0.636}_{0.2} = 34598.4 \text{ MN/m} = \omega^2$

Hence, $\omega = 186$

\[ f = 29 \text{ Hz} \]

Therefore, $S = \frac{\theta}{4 \times 7}$

$T = \frac{0.9}{4 \times 10} = 22.5 \text{ mm}$

So, $N_t = 200 \text{ mm}$

No. of layers = $\frac{200}{22.5} = 8.88$

Taking 8 layers of thickness $T = 25 \text{ mm}$

$S = \frac{200}{4 \times 25} = 2$

\[ f_v = \frac{2 \times 29}{10} = 5.8 \text{ Hz} \]

Assuming thickness of end plate = 25 mm

Total height = $25 \times 2 + 200 + 8 \times 2$

Where, 2mm is the thickness of each rubber shrimp

Hence, Total height = 266 mm

With cover of 5mm

Diameter of steel plate= $900 - 10 = 890 \text{ mm}$

• **Lead rubber bearing parameters**

<table>
<thead>
<tr>
<th>ITEMS</th>
<th>DESIGN VALUE</th>
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<tbody>
<tr>
<td>Diameter of rubber</td>
<td>900 mm</td>
</tr>
<tr>
<td>Thickness of rubber layer</td>
<td>200 mm</td>
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</table>
4) DEVELOPMENT OF MODEL

G+10 storied buildings are modeled using conventional beams, columns and slab. These buildings were given square geometry with plan dimension 16m x 16m. They are loaded with dead, live, wind and seismic forces. These models are then analyzed using response spectrum method for earthquake zone V of India. The details of the modeled building are listed below. Modal damping of 5% is considered, R= 5 and I= 1. The performance of the models were recorded through ETABS to present brief idea about the role of base isolation in protecting the structure against earthquake hazards. The following assumptions were made before the start of modeling procedure so as to maintain similar conditions for both the models:

1) Only main block of the building is considered. The staircase are not considered in the design procedure.
2) At ground floor, slabs are not provided and the floor is resting directly on found.
3) The beams are resting centrally on the column so as to avoid eccentricity.
4) For all structural elements, M25 & Fe415 are used.
5) The footings are not designed. The footings are assigned in the form of either fixed support or link support.
6) Seismic loads are considered in the horizontal direction only (X & Y) and the loads in vertical direction are assumed to be insignificant.

I. Description of models
   • Model 1= fixed base
   • Model 2= isolated base

II. Building details
   • Structure = RCC
   • Structure type = plan regular structure
   • Plan dimension = 16m x 16m
   • Height of building = 30.2m (G+10)
   • Height of each story= 3m except bottom story (3.2m)
   • In X-Direction = 4 bay of 4m
   • In Y-Direction = 4 bay of 4m

III. Material property
   • Grade of concrete = M25
   • Grade of steel = Fe415
   • Density of concrete = 25KN/m^3
   • Density of brick work = 20KN/m^3

IV. Section property
   • Beam size = 300mm X 450mm
   • Column size = 500mm X 500mm
   • Slab thickness = 200mm
   • Wall thickness = 230mm

V. Load consideration
   1) Gravity load
      • Dead load = column, beam, slab
      • Live load= 3KN/m^2

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<table>
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<tr>
<th>Thickness of single rubber layer</th>
<th>25 mm</th>
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<tr>
<td>No. of layers</td>
<td>8 nos.</td>
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<tr>
<td>Height of isolator</td>
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<tr>
<td>Thickness of steel plate</td>
<td>25 mm</td>
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<tr>
<td>Thickness of cover plate</td>
<td>5 mm</td>
</tr>
<tr>
<td>Diameter of steel plate</td>
<td>890 mm</td>
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</table>
- Floor finish = 1KN/m^2

2) Lateral Load of Response Spectrum Analysis
   - Soil Profile type = Medium
   - Seismic Zone Factor = Zone 5
   - Response Reduction Factor = 5.0
   - Importance Factor = 1.0
   - Damping = 5.0

3) Characteristics of Lead Rubber Bearing Isolators are provided above every footing at 0.266m above base level. Properties of LRB are mentioned below:
   - Vertical stiffness (linear) = 771200KN/m
   - Horizontal stiffness (linear) = 1103.7KN/m
   - Horizontal stiffness (Nonlinear) = 11037 KN/m

(DESIGN WINDOW OF ETABS)

(PLAN OF ETABS MODEL)
5) ESTIMATION OF STEEL DIFFERENCE

- **Column steel (isolated base)**
  
  As we see in the designed output that the column steels of both the models are different. So, we will be calculating the required steel.

1) Vertical bars

<table>
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<tr>
<th>COLUMN NOTATION</th>
<th>NO. OF COLUMNS</th>
<th>LENGTH OF BAR</th>
<th>NO OF BARS</th>
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(Vertical reinforcement in isolated base building)

2) Stirrups

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(Vertical reinforcement in isolated base building)
(STIRUPS IN ISOLATED BASE BUILDING)

Hence the total weight of steel required for column of isolated base is 31526.23 Kg.

- **Column steel (fixed base)**
  1. Vertical bar

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**TOTAL= 24550.35**

(VIRTUAL REINFORCEMENT IN FIXED BASE BUILDING)

Hence the total weight of steel required for column of fixed base is 36451.4 Kg

- **Beam steel**

  There is no difference between beam reinforcement in fixed base model and isolated base model
• **Reinforcement steel difference**
  
  The steel difference is as follows:

  \[
  \% \text{ difference} = \frac{\text{steel in fixed base} - \text{steel in isolated base}}{\text{steel in fixed base}} \times 100
  \]

  \[
  \% \text{ difference} = \frac{36451.4 - 31526.33}{36451.4} \times 100
  \]

  \% difference = 13.51

  Cost of steel is decreased by 13.51\% to make it earthquake resistant.

  6) **CONCLUSION**

  • Fixed base model base isolated model by providing lead rubber bearing these two models were analyzed by response spectrum analysis from these building models following conclusions can be made:

  a. Modal displacements are increased in every story after providing LRB which is important to make a structure flexible during earthquake.

  ![Comparison Graph of Story Displacement in Global X Direction](image1.png)

  ![Comparison Graph of Story Displacement in Global Y Direction](image2.png)

  b. Story drift are reduced in higher stories which makes structure safe against earthquake.
c. Story shear reduced after the lead rubber bearing (LRB) is provided as base isolation system which reduces the seismic effect on building.
d. Steel in beam and slab of building remains same.

e. There is change only in the column reinforcement of the structure.

f. The cost of steel is reduced by 13.51% in columns to make it earthquake resistant.

g. Finally it is concluded that after LRB is provided as base isolation system it increases the structures stability against earthquake and reduces reinforcement hence make structure economical.

7) REFERENCES


